Unit Protection
Differential Relays

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Protection Relays

Differential Relays - BASICS

- Note on CT polarity dots
- Through-current: must not operate
- Internal fault: must operate
- The CT currents are matched perfectly on waveforms, no saturation

Differential protection is a fast, selective method of protection against short circuits. It does not need coordination with other relays, however, it lacks to have backup protection.
How can we measure the differential current?
Simply by an overcurrent relay.

Our expectations are:
1- No operation for normal duty of the device
2- No operation for fault outside
3- Operate for a fault inside

The problem is the mismatching of currents:
1- May occur during the normal operation of the device for instant when transformer tap changes
Can be overcome with proper setting of O/C relay
2- Occurs when carrying large outside through fault currents with dc components
This is the main cause of instability (malfunction) of the relay during external fault
**Solution:**
One technique applied to simple overcurrent differential schemes is to use sufficient time delay to ride through the period of CT saturation. Delayed tripping is generally unwanted, so other, more sophisticated techniques are available to provide secure operation for external faults with CT saturation and still provide fast operation for internal bus faults.

1- Using stabilizing resistor in circuit

2- Using Biased relays

This is the most Popular Scheme
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Where do they use? The followings are just some examples:

Generators - Motors

Transformers

Busbars

The schematics shown are examples of differential protection schemes.
1- Using stabilizing resistor:

a) Low Impedance Differential Protection:

Under external fault condition, the protection must remain stable and should not operate, even if one C.T. has completely saturated. A series resistor Rs can be inserted in series with the relay so that the current passing through the relay is less than its operating current under the maximum through fault current:

\[ I_{\text{Set}} > \frac{I_F}{N} \frac{(R_{CT} + R_t)}{R_r + R_s + R_{CT} + R_t} \]
b) High Impedance Differential Protection:

The high-impedance input is created by an internal impedance, typically resistive, of 2000 ohms or higher. A sensitive current element in series with the high-impedance element is calibrated in volts based on the voltage drop across the internal impedance.

Metal Oxide Varistor (MOV) is used to prevent the danger of the over voltage that will be produced when fault is inside the protected area.
High Impedance Differential Relay

High-impedance differential relays are typically used for bus protection.

Bus protection is an application that demands many sets of CT’s be connected to the relays. It is also an application that demands the relay be able to operate with unequal CT performance, since external fault magnitudes can be quite large. The high impedance differential relay meets both requirements.

Also note that a voltage-limiting MOV connected across the high-impedance relay is shown in the figure. This is to keep the voltage less than a specified value (usually less than CT knee point voltage). MOV prevents the high voltage to be built up across the CT during internal fault and so preventing the relay and the CTs from damaging.
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Differential Relays

\[ V_r = V_t = \frac{I_F}{N} \cdot (R_{CT} + R_I) \]

\[ K = \text{Safety Factor} = 1.5 \]

\[ V_{\text{pickup}} = K \cdot V_r \]

\[ R_r = R_s >> R_{CT} + R_I \]

Equation 1: For internal fault current

Equation 2: For through fault current
2- Using Biased relay:
This is designed to respond to the differential current in the term of its fractional relation to the current flowing through the protected section. In this type of relay, there are restraining coils in addition to the operating coil of the relay. The restraining coils produce torque opposite to the operating torque. Under normal and through fault conditions, restraining torque is greater than operating torque. Thereby relay remains inactive. When internal fault occurs, the operating force exceeds the bias force and hence the relay is operated. This bias force can be adjusted by varying the number of turns on the restraining coils. As shown in the figure below, if $I_1$ is the secondary current of CT, and $I_2$ is the secondary current of CT, then current through the operating coil is $I_1 - I_2$ and current through the restraining coil is $(I_1 + I_2)/2$. In normal and through fault condition, torque produced by restraining coils due to current $(I_1 + I_2)/2$ is greater than torque produced by operating coil due to current $I_1 - I_2$ but in internal faulty condition these become opposite. And the bias setting is defined as the ratio of $(I_1 - I_2)$ to $(I_1 + I_2)/2$.

It is clear from the above explanation, greater the current flowing through the restraining coils, higher the value of the current required for operating coil to be operated. The relay is called percentage relay because the operating current required to trip can be expressed as a percentage of through current.

$$Bias\ setting\ in\ percentage = \frac{I_1 - I_2}{(I_1 + I_2)/2} \times 100\%$$
Differential Relays

Setting:

- $I_d >$ setting depends to the nominal current with considering: Transformer maximum tap change, cable capacitive current, Mismatching of CTs, No load magnetizing current

- Slope $K_1$ together with its base point counts for current proportional false current due to CT errors about 20-25%

- Slope $K_2$ together with its base point counts for CT saturation, setting is about 40-50%

- $I_d >>$ works without restrain and designed for high internal fault currents on the primary side of the transformer with a high degree of CT saturation. It should be set to at least 20% above the max. through flowing fault current or the max. inrush currents, whichever is bigger.
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Three phase Differential Relays – How fault current flows

Generator Phase to Phase Fault

12
Protection Relays

Three phase Differential Relays – How fault current flows

Generator External Fault

Diagram showing the flow of fault current in a generator external fault scenario.
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Phase Correction in Transformer Protection

- For different transformer vector group, phase correction must be implemented.
- Electromechanical and static relays use appropriate CT connections to ensure that the primary and secondary currents applied to the relay are in phase.
- For digital and numerical relays, it is common to use star connected line CT’s on all windings of the transformer and compensate for the winding phase shift in software. The only data required is the transformer vector group designation. Phase compensation is then performed automatically.

Use of Interposing CT
The formula for phase compensation in digital relays:

\[ \left( \begin{array}{l} I_a^* \\ I_b^* \\ I_c^* \end{array} \right) = \frac{2}{3} \left( \begin{array}{ccc} \cos(k - 30) & \cos[(k + 4).30^\circ] & \cos[(k - 4).30^\circ] \\ \cos[(k - 4).30^\circ] & \cos(k.30^\circ) & \cos[(k + 4).30^\circ] \\ \cos[(k + 4).30^\circ] & \cos[(k - 4).30^\circ] & \cos(k.30^\circ) \end{array} \right) \cdot \left( \begin{array}{l} I_a \\ I_b \\ I_c \end{array} \right) \]

K is the transformer vector group.
It will be applied after filtering the zero sequence current.
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**Differential Relays**

**Transformer inrush current**

The phenomena of inrush current is fully described in Appendix VI

An inrush current with a high proportion of \(2^{nd}\) harmonics is generated when switching the transformer on, which can lead to false tripping of the differential protection. The preset value for the inrush restraint with \(2^{nd}\) harmonics of 15% can be accepted unchanged. A lower value can be set for greater restraint in exceptional cases under unfavorable energizing conditions resulting from the design of the transformer.

The inrush restraint can be extended by the cross-block function. This means, that all three phases of the \(I_{Diff}\) stage are blocked when the harmonic component is exceeded in only one phase. A setting value of 3 periods, effective for the time of mutual blocking after exceeding the differential current threshold, is recommended (preset).
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Biased differential protection for three-winding transformer

Three winding transformer (three power sources)

Biased differential protection for three-winding transformer

Three-winding transformer with unloaded delta tertiary
Transformer earth fault protection: Restricted Earth Fault (REF) 64

The same philosophy as differential protection will be used in REF. Here we compare the 3I0 going through the earth with that residual current of the line:
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Generator REF protection

Diagram of Stator Winding and Relay circuits.
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Solidly earthed and resistor grounded single phase fault current: REF protection
Other areas of concern

- Over-current
- Gas detection
  - Faults give rise to generation of gas
    - Slow for minor faults
    - Violent for heavy faults
- Overheating
  - Oil
  - Winding
Bochholz Relay

Very slow to act on fault, just backup for overloading
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Oil Temp / Winding Temp Indicator
Low Impedance Differential Relay

A 11 kV busbar with four outgoing circuits is protected by a low impedance differential protection system on each phase. The CT used has a ratio of 400/1 and a d.c. winding resistance of 0.5 Ω. The current setting of the relay used is 1A and consume 1VA under rated current. The maximum fault current for a busbar fault is 6000 A.

Calculate the value of the series resistor that can be inserted in series with the relay in order to prevent mal-operation under the maximum through fault current.

When there is no series resistor:

\[
I_r = \frac{I_E}{N} \left( R_{ct} \right) = \frac{6000 \times 0.5}{400 \times (1 + 0.5)} = 5 \text{ A}
\]

Relay will operate

When there is a series resistor, let the max current through relay is 0.5 A when one CT saturates on external fault

\[
I_r = \frac{I_E}{N} \left( R_{ct} \right) = \frac{6000 \times 0.5}{400 \times (1.5 + R_s)} = 0.5 \text{ A},
\]

\[
R_s = 13.5 \Omega \text{ to prevent relay operate on through fault.}
\]
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Differential Relays Example

High Impedance Differential Relay Example

Given $R_{CT}=2\Omega$, $R_f=0.46\Omega$, maximum fault level of the 132 kV plant =6000 MVA

Knee point of CT=380V, CT ratio=600/1

Magnetizing current of CT at 120V=0.015A

MOV current at setting=0.02A

Stabilizing shunt resistor=200Ω

Choose the setting of the relay and calculate the primary fault setting

Max through fault current

$$I_f = \frac{6000 \times 10^6}{\sqrt{3 \times 132 \times 10^3}} = 26243 A$$

$$V_f = \frac{26243}{600} \times (2+0.46) = 108 V$$

Vset = 1.5 x 108 = 162V

$162 < MOV\ voltage < 380\ V$

Primary fault setting = $600 \times \left[ 0.015 \times 2 + 0.02 + \frac{162}{200} \right] = 516\ A$

This means that if the internal fault current is bigger than 516A the relay will operate.
Biased differential Relay model and example:

**Example**

Transformer = 420MVA, 530kV/23kV, 17.4%
Tap changer = 21 taps, nominal tap = tap 9
HV voltage at maximum tap = 450.5kV indeed 450.5kV/23 kV
(The tap specified means: we have 0-1-2----9------21 tap number positions then 530-450.5=79.5*100/530=15%
therefore each tap is 15%/12=1.25% **maximum** (minimum) tap is -15% and **minimum** (maximum) tap is 1.25*9=11.25%)

anguage
CTRHV = 1500/1, CTRLV = 19000/1
At nominal tap:
I FLLV = 420*1000/(1.73*23) = 10543A primary or /19000
=0.555 A in secondary
Ct correction = 19000*23/1500*530=0.55
We will set this value or digital relays calculate that from network specifications that are entered.
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Differential Relays Example

I_{FLHV} = 420 \times 1000/(1.73 \times 530) = 457.5 \text{ primary or } /1500 \times 0.55 = 0.555 \text{ A in secondary}
I_{FLHV_{\text{inmaxtap}}} = 420 \times 1000/(1.73 \times 450.5) = 539 \text{ A primary or } /1500 \times 0.55 = 0.655 \text{ A in secondary}
I_{FLHV_{\text{inmintap}}} = 420 \times 1000/[1.73 \times (530 + 0.1125 \times 530)] = 411.26 \text{ A primary or } /1500 \times 0.55 = 0.495 \text{ A in secondary}

\text{a) } I_{\text{dif}}:\n\text{Id} > 0.555 - 0.655 = -0.1
\text{Id} > 0.555 - 0.495 = 0.06

Therefore \text{id} > 0.1 \text{ or } 10\% \text{ Let put a 2\% margin then it is 12\%.}

\text{b) Slope 1: Assume type A relay (ITOT = I_{\text{res}}):}
K_1 = \text{Idif/I_{\text{res}}} = 0.1/0.5 \times (0.555 + 0.655) = 0.17 \text{ or 17\% then a 20\% setting is good.}
PT_1 = 0.5 \times (0.555 + 0.655) = 0.605 \text{ A}

\text{C) Turning Point 2, ITP2 Slope 1 dictates the relay restraint characteristic over the load current range of the transformer.}
\text{Thus it is meant to be effective up to the maximum possible loading of the transformer.}
\text{For large power transformers this could be up to 200\% of rated current.}
\text{For smaller transformers allowable maximum loading could be anything from 100\% to 200\% of rated load typically 150\%.}
\text{For most cases a turning point of 2 (corresponding to twice rated load) suffices.}
\text{Again assume type A: I_{\text{res}} at PT2 = 2 \times I_{\text{FLres}} = (0.655 + 0.555) \times 2 = 2.42 \text{ A}}
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Differential Relays Example

d) Slope 2: The second bias slope is intended to ensure additional restraint with severe through fault currents that could lead to CT saturation. 
Assuming that the CT saturation will occur for the through fault current then: \( ILV = 0 \)
For Type A:

\[
Idif = 20(IHV) \\
Ires = 20*0.5*(IHV)
\]

\[
K2 = 1/0.5 = 200\%
\]

e) \( Id>> \) will set like instantaneous for over current relays. We need to have fault current for fault at the primary side of transformer. Then \( Id>> \) will be calculated